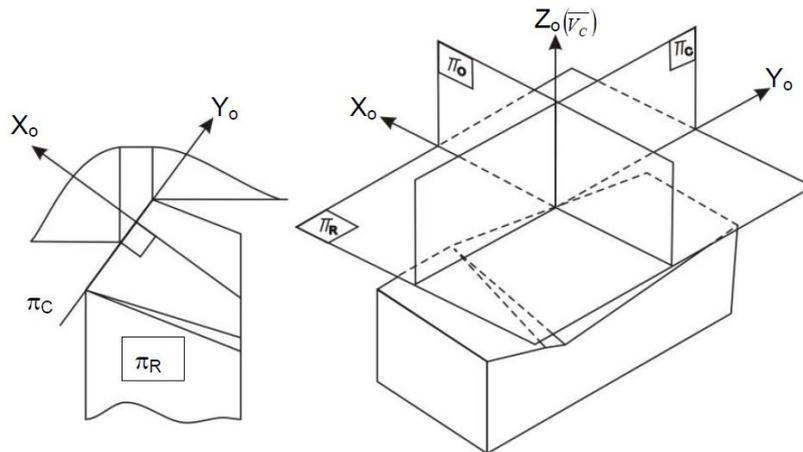


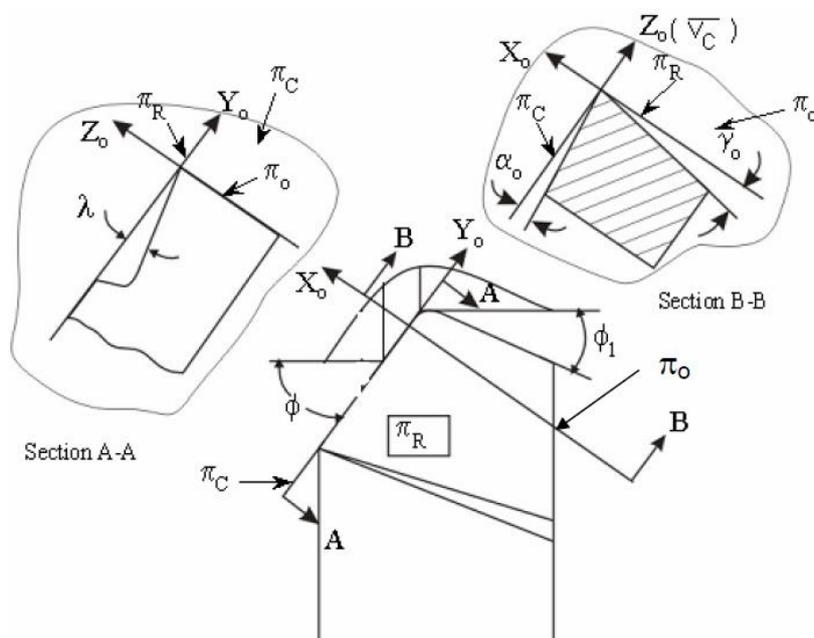
Design of Tool Geometry

2.2.2.2 Designation of tool geometry in the orthogonal rake system(ORS)

This system is also known as ISO - old. The planes of reference and the co-ordinate axes used for expressing the tool angles in ORS are: π_R - π_C - π_O and X_o - Y_o - Z_o which are taken in respect of the tool configuration as indicated in Fig



where, π_R = Reference plane perpendicular to the cutting velocity vector, π_C = cutting plane; plane perpendicular to π_R and taken along the principal cutting edge π_O = Orthogonal plane; plane perpendicular to both π_R and π_C and the axes; X_o = along the line of intersection of π_R and π_O Y_o = along the line of intersection of π_R and π_C Z_o = along the velocity vector, i.e., normal to both X_o and Y_o axes. The main geometrical angles used to express tool geometry in Orthogonal Rake System (ORS) and their definitions will be clear from Fig



1.Rake angle

Rake angles [Fig. 3.7] in ORS

γ_o = orthogonal rake: angle of inclination of the rake surface from Reference plane, πR and measured on the orthogonal plane, π_o

λ = inclination angle; angle between πC from the direction of assumed longitudinal feed [πX] and measured on πC

2.clearance angle

α_o = orthogonal clearance of the principal flank: angle of inclination of the principal flank from πC and measured on π_o
 α_o' = auxiliary orthogonal clearance: angle of inclination of the auxiliary flank from auxiliary cutting plane, $\pi C'$ and measured on auxiliary orthogonal plane, π_o'

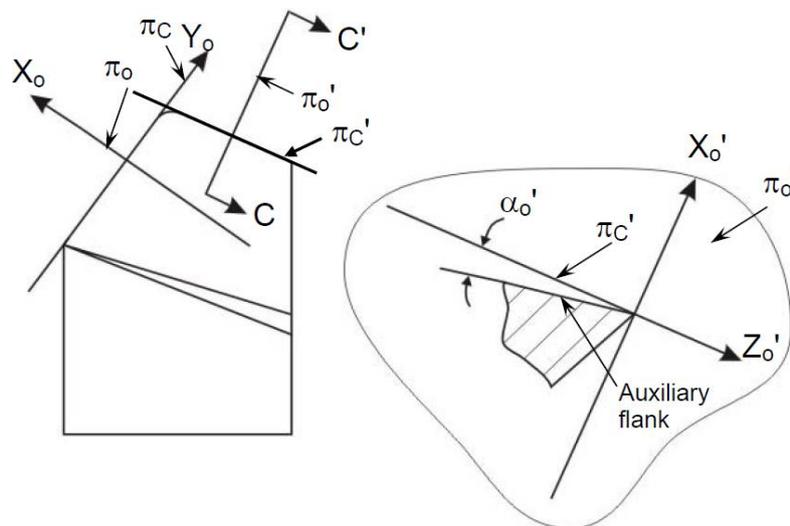
3.Cutting angles

ϕ_1 = principal cutting edge angle: angle between πC and the direction of assumed longitudinal feed or πX and measured on πR

ϕ_1' = auxiliary cutting angle: angle between $\pi C'$ and πX and measured on πR

4. Nose radius

r (mm) r = radius of curvature of tool tip



2.2.2.3 Designation of tool geometry in the normal rake system(NRS)

This system is also known as ISO – new. ASA system has limited advantage and use like convenience of inspection. But ORS is advantageously used for analysis and research in machining and tool performance. But ORS does not reveal the true picture of the tool geometry when the cutting edges are inclined from the reference plane, i.e., $\lambda \neq 0$. Besides, sharpening or re

sharpening, if necessary, of the tool by grinding in ORS requires some additional calculations for correction of angles.

These two limitations of ORS are overcome by using NRS for description and use of tool geometry. The basic difference between ORS and NRS is the fact that in ORS, rake and clearance angles are visualized in the orthogonal plane, π_o , whereas in NRS those angles are visualized in another plane called Normal plane, π_N . The orthogonal plane, π_o is simply normal to π_R and π_C irrespective of the inclination of the cutting edges, i.e., λ , but π_N (and $\pi_{N'}$ for auxiliary cutting edge) is always normal to the cutting edge. The differences between ORS and NRS have been depicted in Fig. The planes of reference and the coordinates used in NRS are: π_{RN} - π_C - π_N and X_n - Y_n - Z_n where, π_{RN} = normal reference plane π_N = Normal plane: plane normal to the cutting edge and $X_n = X_o$ $Y_n = Y_o$ $Z_n = Z_o$ It is to be noted that when $\lambda = 0$, NRS and ORS become same, i.e. $\pi_o \cong \pi_N$, $Y_n \cong Y_o$ and $Z_n \cong Z_o$

1.Rake angle

γ_n = normal rake: angle of inclination angle of the rake surface from π_R and measured on normal plane, π_N α_n = normal clearance: angle of inclination of the principal flank from π_C and measured on π_N α_n' = auxiliary clearance angle: normal clearance of the auxiliary flank (measured on $\pi_{N'}$ - plane normal to the auxiliary cutting edge. The cutting angles, ϕ and ϕ_1 and nose radius, r (mm) are same in ORS and NRS.